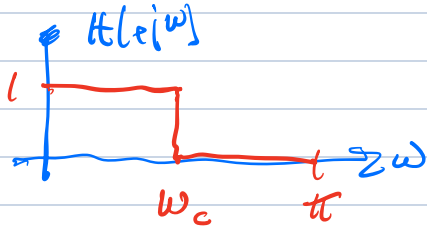


3/25/24

INTRO TO DIGITAL FILTER DESIGN

(OYSP 7.0-7.3)

IDEAL FILTERS



CFTT

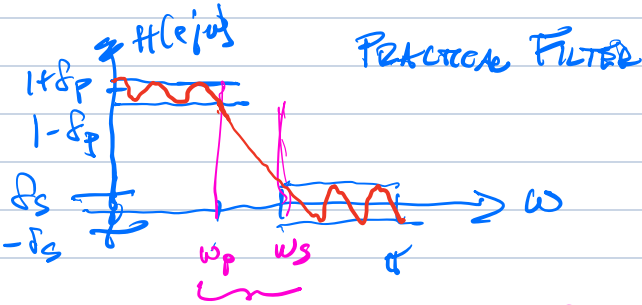
$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega) e^{j\omega t} d\omega$$

$$X(j\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

DTFT

$$x[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) e^{j\omega n} d\omega$$

$$X(e^{j\omega}) = \sum_{n=-\infty}^{\infty} x[n] e^{-j\omega n}$$

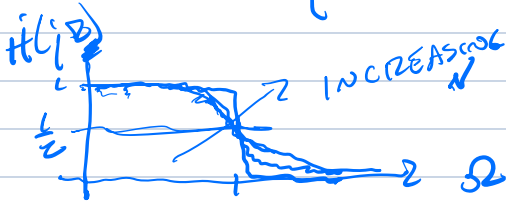


$\Delta\omega = \omega_s - \omega_p$ TRANSITION BANDWIDTH

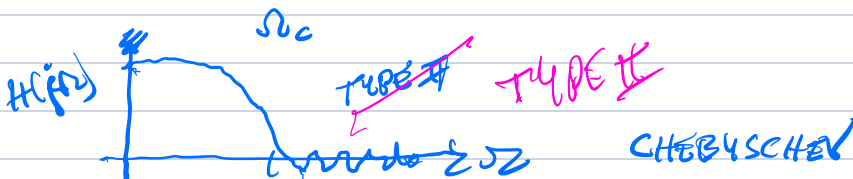
GOAL: FOR IIR DESIGN CONVERT A "GOOD" CT IIR DESIGN INTO A "GOOD" DT DESIGN

1. WHAT IS "GOOD"?
2. HOW TO DO CONVERSION

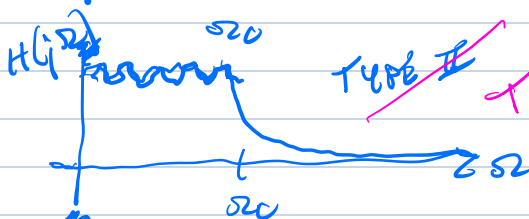
EXAMPLES OF "GOOD" CT DESIGNS



BUTTERWORTH



CHEBYSHEV

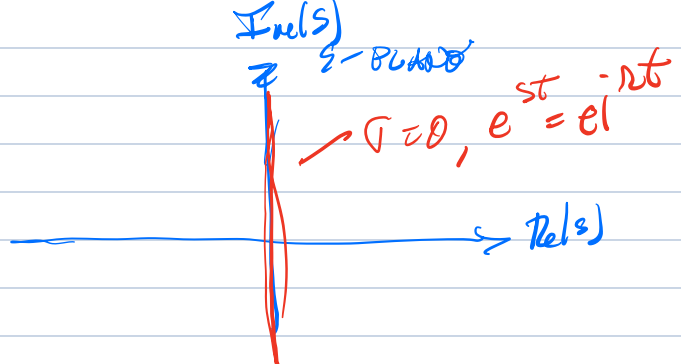


ELLIPTIC FILTER

LAPLACE U. Z-TRANSFORMS

$$e^{st}, s = \sigma + j\omega$$

$$e^{(\sigma + j\omega)t} = e^{\sigma t} e^{j\omega t}$$

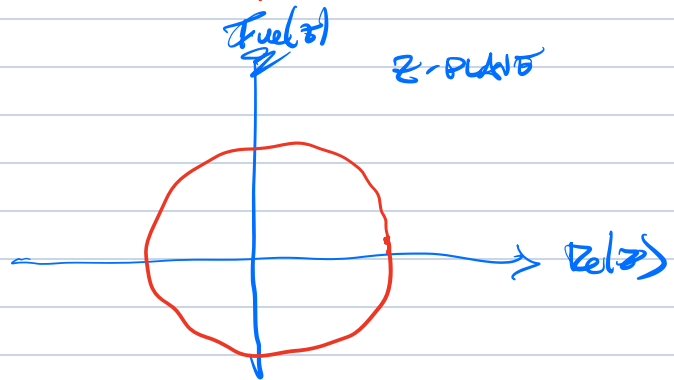


S-PLANE Z-PLANE

$$j\omega\text{-AXIS} \iff |z| = 1$$

$$\text{LEFT HALF of S-PLANE} \iff |z| < 1$$

$$\text{RIGHT HALF of S-PLANE} \iff |z| > 1$$



POSSIBLE MAPPINGS of S-PLANE TO Z-PLANE

$$h_c(t) \rightarrow h_d(z) \quad \text{IMPULSE INVARIANCE}$$

$$\star s_c(t) \rightarrow s_d(z) \quad \text{STEP INVARIANCE}$$

$$\star \text{DIFF. EQ.} \rightarrow \text{DIFF. EQ.} \quad \text{DIFF EQS}$$

$$H_c(s) \rightarrow H_d(z) \quad \text{BILINEAR TRANSFORMATION}$$

QUESTIONS ABOUT MAPPINGS:

$$\star \text{STABLE IN CT} \rightarrow \text{STABLE IN DT?}$$

$$\star \text{FREE RESP IN CT} \rightarrow \text{FREE RESP IN DT?}$$

MAPPING FROM CT TO DT

METHOD I IMPULSE INVARIANCE

let $h[n] = T h_c(t) \Big|_{t=nT}$

Consider $h_c(t) = e^{s_k t} u(t)$

$$H(s) = \int_{-\infty}^{\infty} h_c(t) e^{-st} dt = \int_{-\infty}^{\infty} e^{s_k t} u(t) e^{-st} dt$$

$$= \int_0^{\infty} e^{t(s_k - s)} dt = \frac{1}{s_k - s} \left[e^{t(s_k - s)} \right]_{t=0}^{\infty}$$

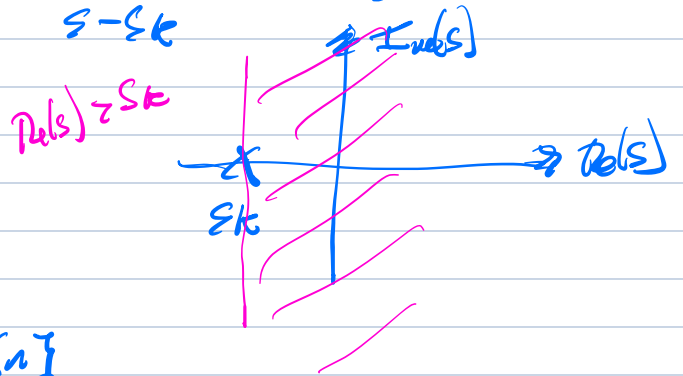
$\text{Re}[s_k - s] < 0$

$$= \frac{1}{s_k - s} [0 - 1] = \frac{1}{s - s_k}, \quad \text{Re}[s_k - s] < 0$$

$h[n] = T h_c(t) \Big|_{t=nT} = T e^{s_k nT}$

$$= T e^{s_k nT} = T (e^{s_k T})^n u[n]$$

$$H(z) = \sum_{n=-\infty}^{\infty} h[n] z^{-n} = T \sum_{n=0}^{\infty} (e^{s_k T})^n z^{-n} = \frac{T}{1 - e^{s_k T} z^{-1}}$$



STABLE IN S-PLANE IF $\text{Re}(s_k) < 0$

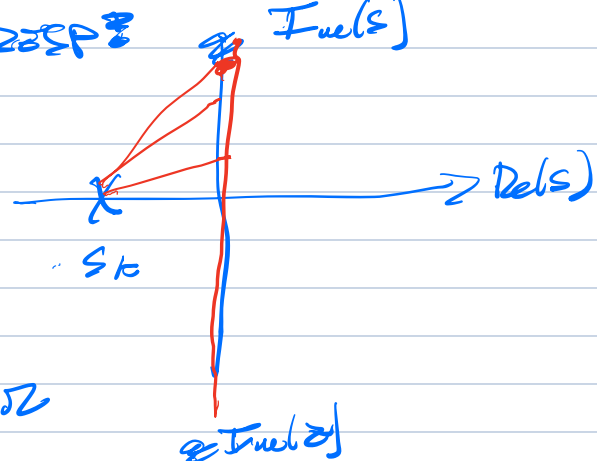
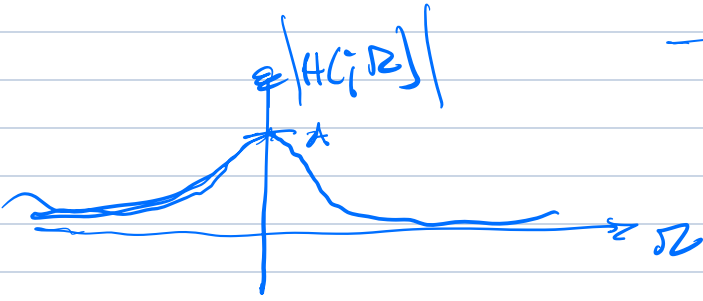
IN Z-PLANE $z_k = e^{s_k T} = e^{(\sigma + j\omega)T} = e^{\sigma T} \cdot e^{j\omega T}$

IF $\sigma < 0, \Rightarrow |z_k| < 1$

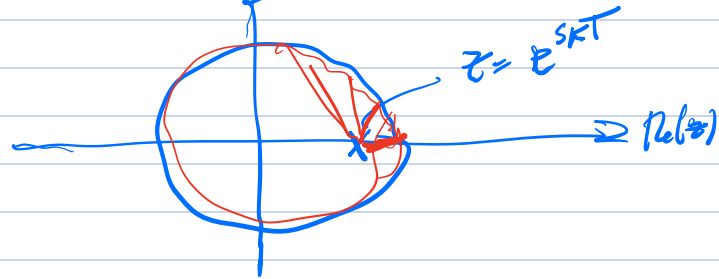
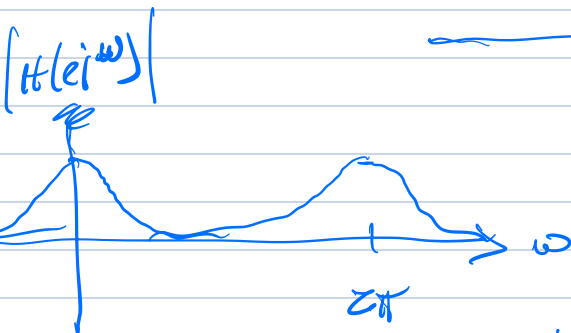
STABLE IN S \Rightarrow STABLE IN Z

WHAT ABOUT FREQ RESP?

ω s-PLANE

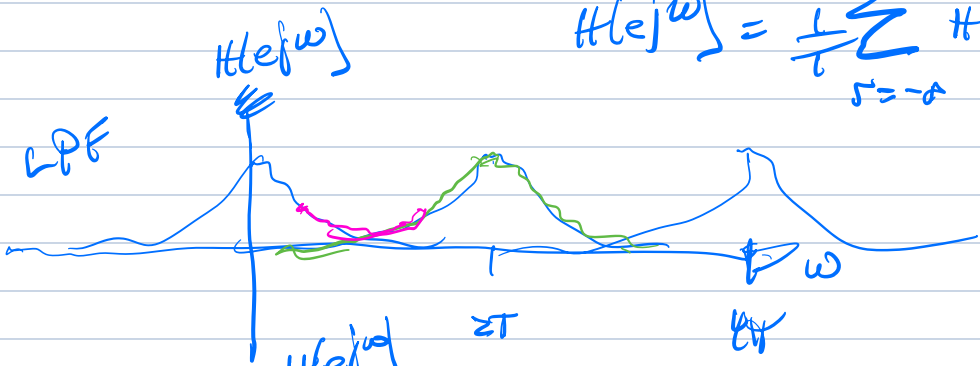


ω DT, z-PLANE

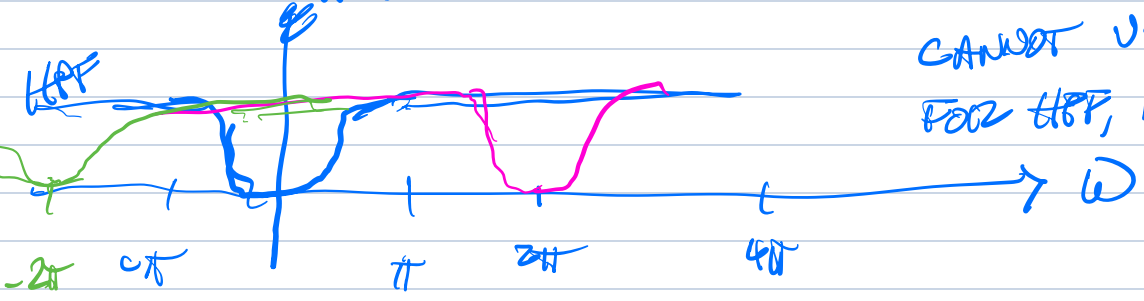


$$H(e^{j\omega}) = \frac{1}{T} \sum_{s=-\sigma}^{\sigma} H(s) \left(e^{j\omega T} - \frac{2\pi n T}{T} \right)$$

LPF

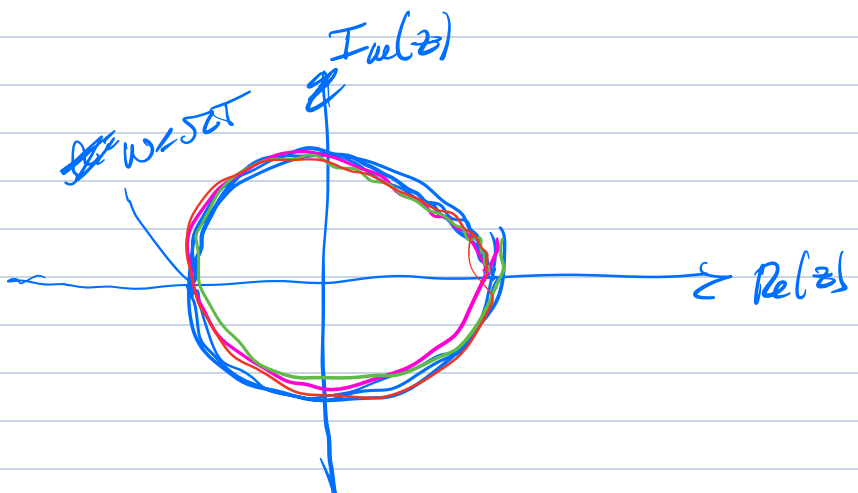


HPF



CANNOT USE FOR HPF, NOTCH FILTERS ETC.

~~ω = 50T~~
ω = 50T



$$\omega = 50T$$

CAN WE MAP $j\Omega$ -AXIS OF s -PLANE INTO
UNIT CIRCLE OF z -PLANE ONCE??

THE BILINEAR TRANSFORM

CONSIDER
$$s = z \frac{1-z^{-1}}{1+z^{-1}}$$

$$s = z \frac{z-1}{z+1}$$

$$s(z+1) = z(z-1)$$

$$z(st-z) = -st-z$$

$$z = \frac{-s-z}{st-z} = \frac{z+st}{z-st} = \frac{1 + \frac{st}{z}}{1 - \frac{st}{z}}$$

let $s = j\Omega \Rightarrow z = \frac{1 + j\frac{\Omega T}{2}}{1 - j\frac{\Omega T}{2}}$

$$|z|^2 = \frac{|1 + j\frac{\Omega T}{2}|^2}{|1 - j\frac{\Omega T}{2}|^2} = \frac{1 + |\frac{\Omega T}{2}|^2}{1 + |\frac{\Omega T}{2}|^2}$$

$j\Omega$ -AXIS IN s MAPS TO UNIT CIRCLE IN z

Now let $s = \sigma + j\omega$

$$z = \frac{1 + \frac{sT}{2}}{1 - \frac{sT}{2}} = \frac{1 + (\sigma + j\omega)\frac{T}{2}}{1 - (\sigma + j\omega)\frac{T}{2}} = \frac{\frac{1+\sigma T}{2} + j\frac{\omega T}{2}}{1 - \frac{\sigma T}{2} - j\frac{\omega T}{2}}$$

$$|z|^2 = \frac{\left(\frac{1+\sigma T}{2}\right)^2 + \left(\frac{\omega T}{2}\right)^2}{\left(1 - \frac{\sigma T}{2}\right)^2 + \left(\frac{\omega T}{2}\right)^2}$$

LHP s-PLANE

$$\sigma < 0$$

⇒ INSIDE of U.C.

How DOES j ω -AXIS MAP INTO UNIT CIRCLE?

$$s = z \frac{1-z^{-1}}{1+z^{-1}}$$

$$s = j\omega$$

$$z = e^{j\omega T}$$

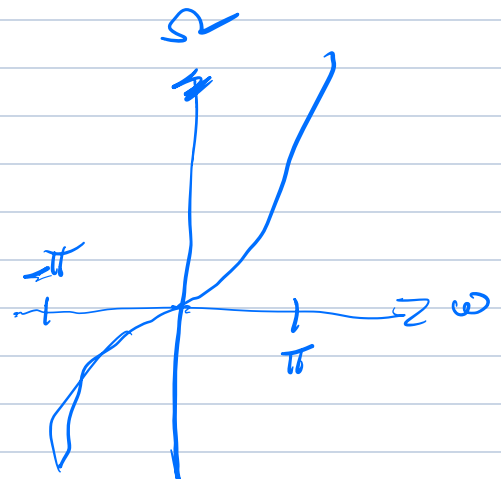
$$j\omega = z \frac{1 - e^{-j\omega T}}{1 + e^{-j\omega T}}$$

$$j\omega = z \frac{e^{j\omega T/2} (e^{j\omega T/2} - e^{-j\omega T/2})}{e^{-j\omega T/2} (e^{j\omega T/2} + e^{-j\omega T/2})} =$$

$$j\omega = z \frac{z^{1/2} \sin(\frac{\omega T}{2})}{z \cos(\frac{\omega T}{2})}$$

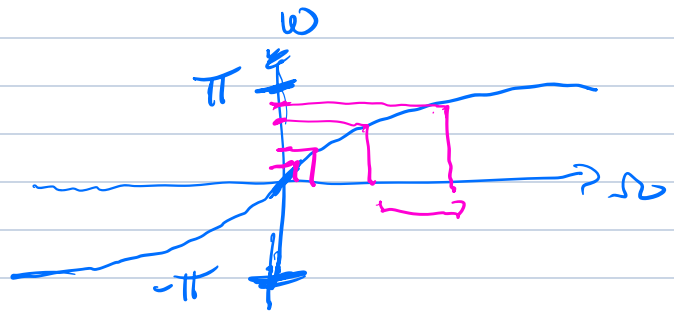
$$\omega = z \tan\left(\frac{\omega T}{2}\right)$$

$$\frac{\omega T}{2} = \tan^{-1}\left(\frac{\omega T}{2}\right)$$



$$\tan^{-1}\left(\frac{\Omega T}{2}\right) = \frac{\omega}{2}$$

$$\omega = 2 \tan^{-1}\left(\frac{\Omega T}{2}\right)$$



X SMALL

$$\sin(x) \approx x$$

$$\tan(x) \approx x$$

$$\cos(x) \approx 1$$

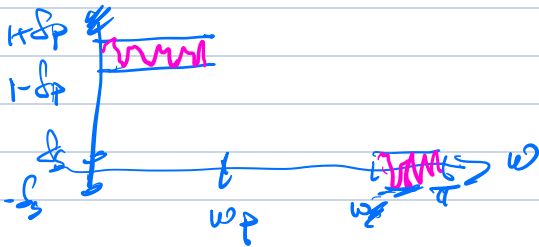
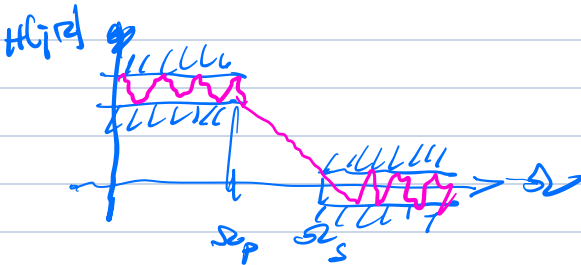
$$\tan^{-1}(x) \approx x$$

FOR
|omega| SMALL

$$\omega \approx \left(\frac{\Omega T}{2}\right)$$

$$\omega \approx \Omega T$$

APPLICATION TO FILTER DESIGN



$$H_c(\Omega) \rightarrow H(e^{j\omega})$$

USING BLT

$$\omega = 2 \tan^{-1}\left(\frac{\Omega T}{2}\right)$$

$$\Omega = \frac{2}{T} \tan\left(\frac{\omega}{2}\right)$$