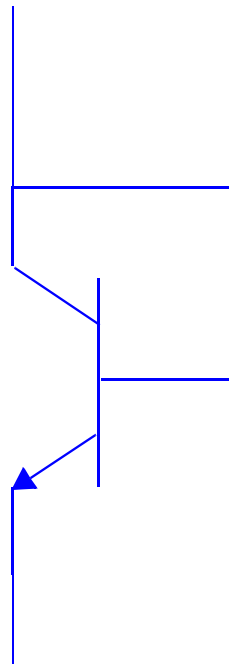
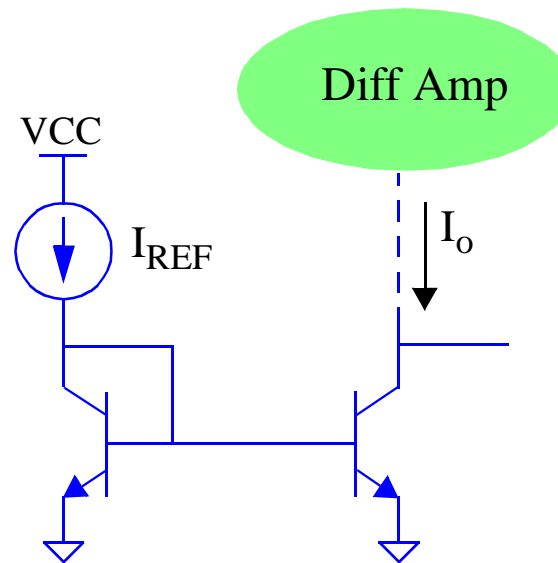


# Diode-connected BJT



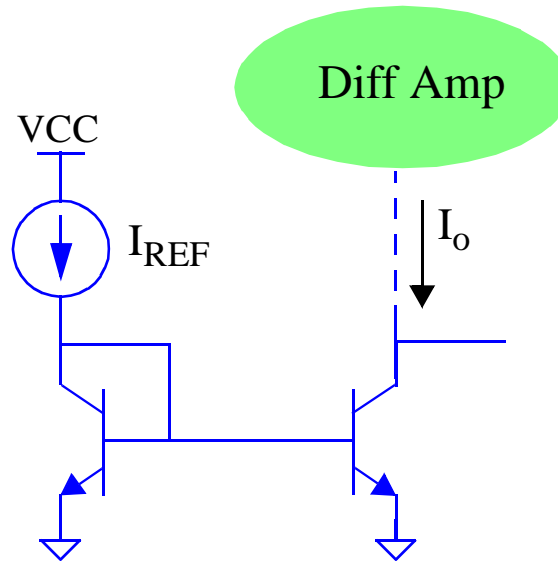
# Current Mirrors

- Current sources are created by mirroring currents
- Example: with infinite  $\beta$ ,  $I_o = I_{REF}$



# Current Mirrors

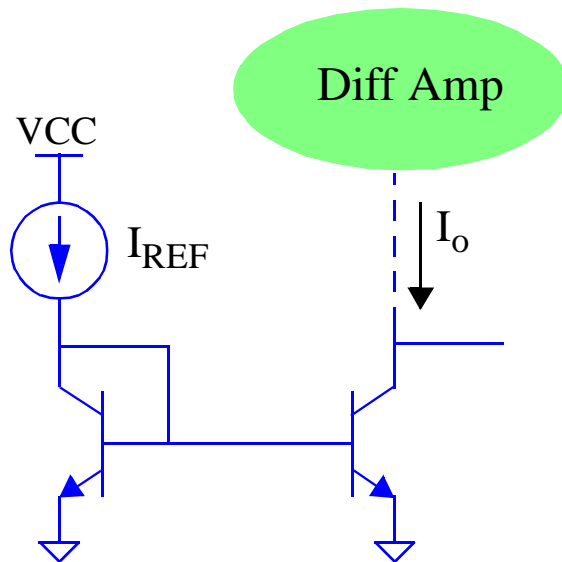
- Example: with finite  $\beta$



- What is the other reason for  $I_{REF} \neq I_o$ ?

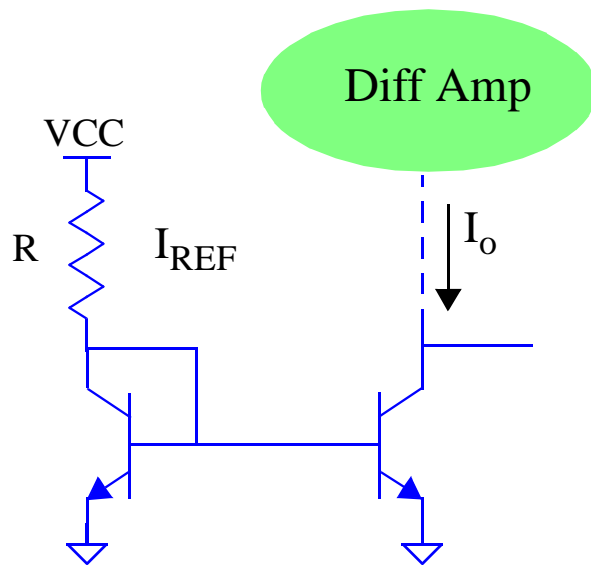
## Output Resistance of Current Source, R

- What is the small signal output resistance of this current source, and why do we care?



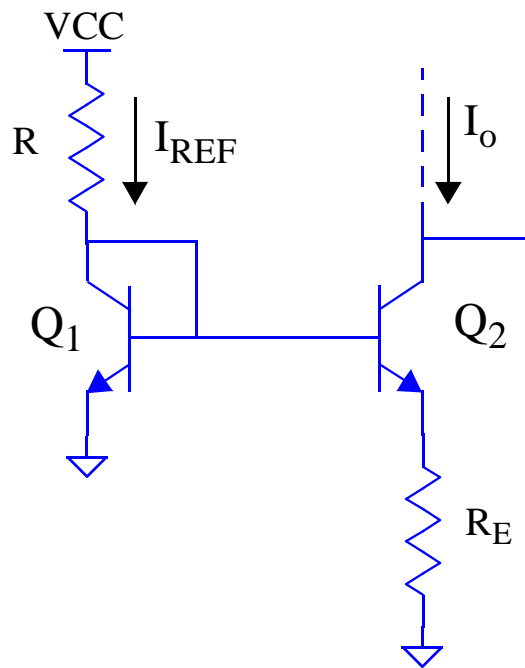
## Simple $I_{REF}$ Model

- Select  $R$  to establish the required reference current



## Widlar current source

- For a given  $V_{CC}$ , you need large resistor  $R$  values to obtain small current!
- Large resistors are expensive, Widlar current source uses smaller resistor in emitter to reduce achieve the same current?



$$I_O R_E = V_{BE1} - V_{BE2}$$

$$V_{BE1} = V_T \ln(I_{REF}/I_S)$$

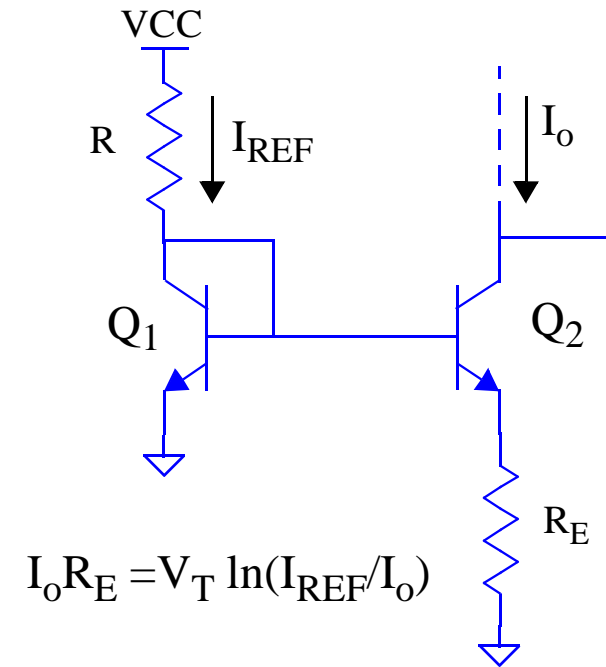
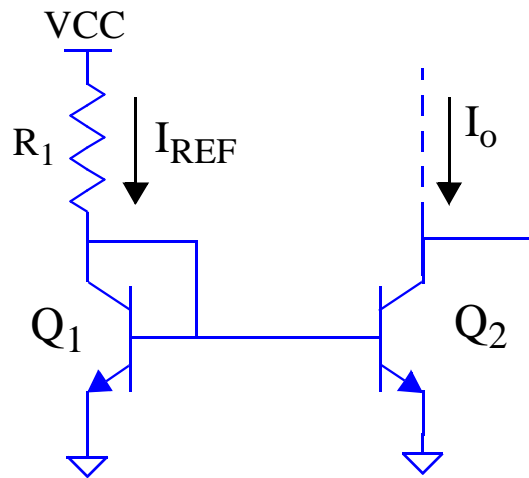
$$V_{BE2} = V_T \ln(I_O/I_S)$$

$$V_{BE1} - V_{BE2} = V_T \ln(I_{REF}/I_O)$$

$$I_O R_E = V_T \ln(I_{REF}/I_O)$$

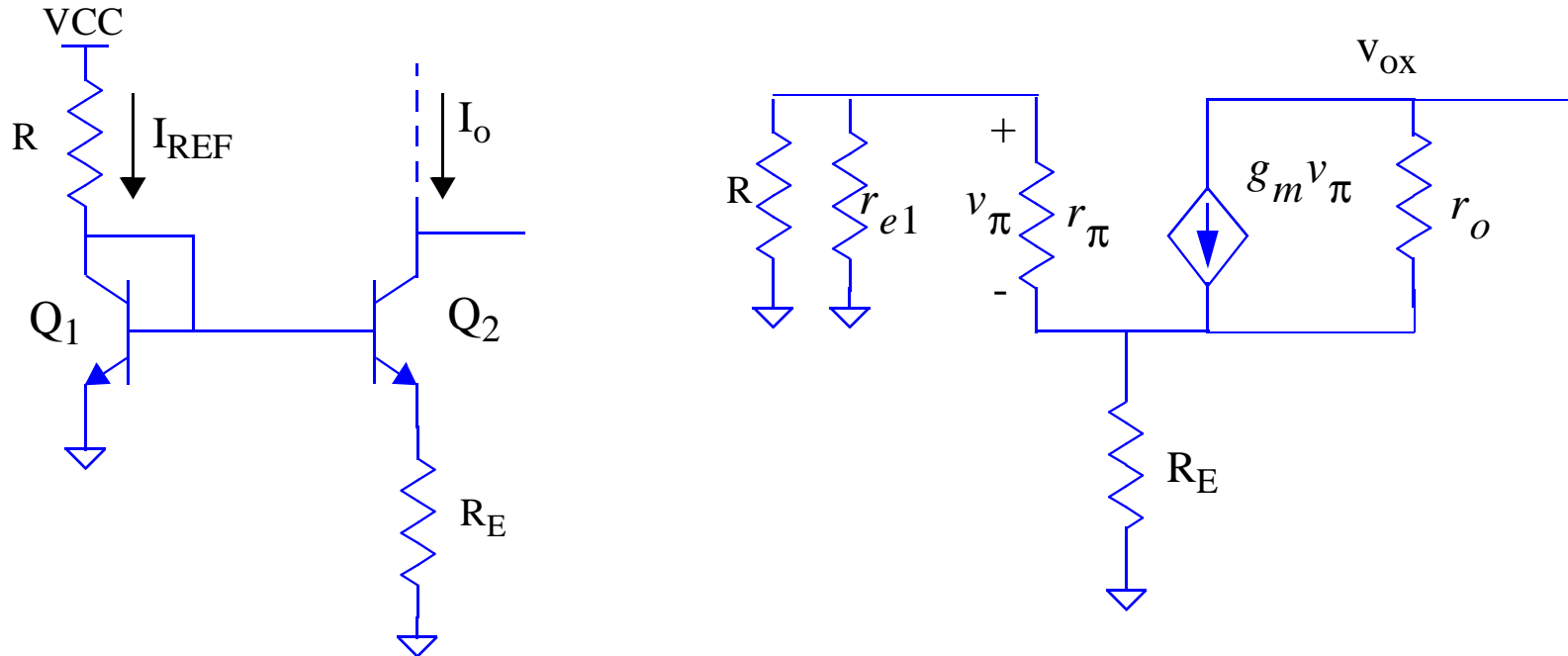
## Widlar current source vs. ordinary current mirror

- Let us say we need  $I_o = 10\mu\text{A}$
- Assume that for  $I = 1\text{mA}$   $V_{BE} = 0.7$



## Widlar current source - output resistance

- If we neglect  $R \parallel r_{e1}$ , base of  $Q_2$  is on ac ground

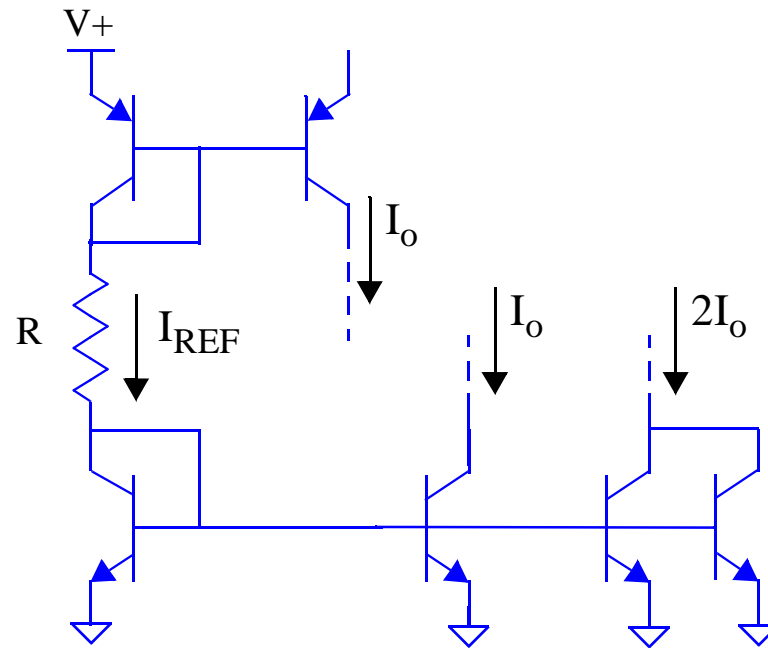


- Presence of  $R_E$  is increases output resistance to  $(1+g_m R_E \parallel r_\pi)r_o$ .  
(Read Sec. 6.4 in the textbook!)



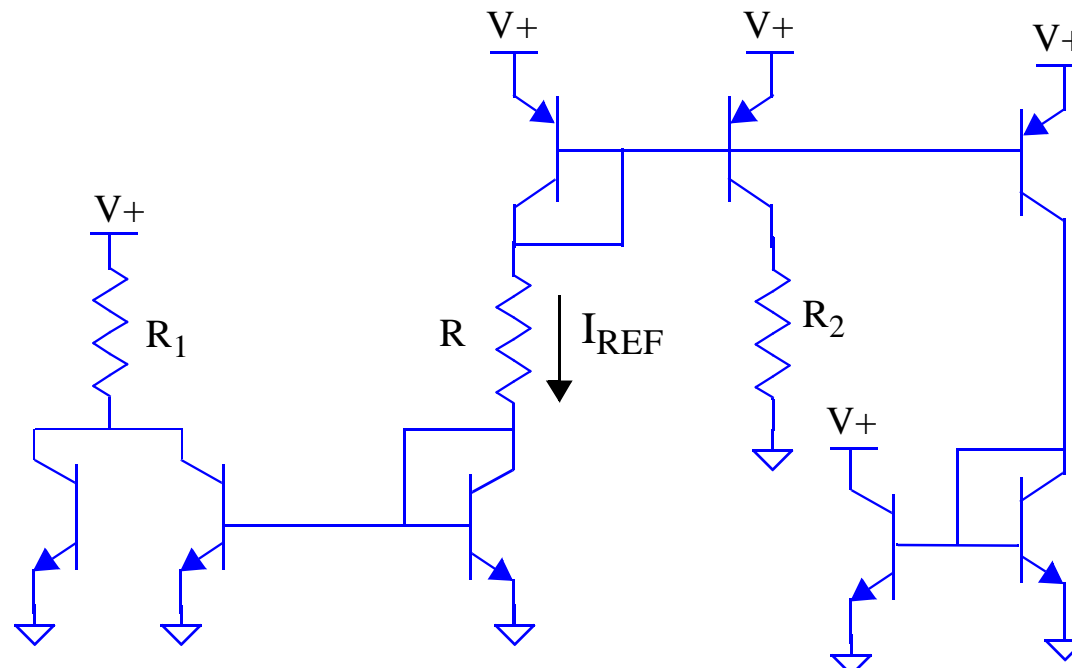
# Current Steering

- With an  $I_{REF}$  established, steer and/or scale the reference value



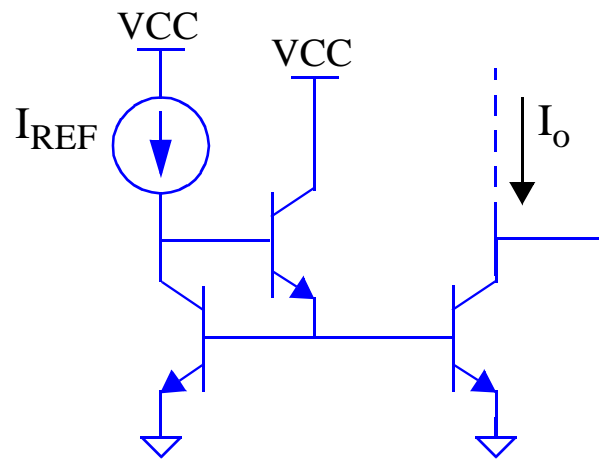
## Reading IC circuit schematics

- Find a path between + power supply and - power supply which sets the reference current (very often there is only one even in a large circuit): Only  $V_{BE}$  and resistors are in this path.
- Type of transistor will tell you the expected direction of current: npn - current sink, pnp - current source.
- Identify current mirror configurations (Widlar, Wilson, etc.) and respective emitter areas.
- Proceed from the reference current branch and calculate subsequent currents independently



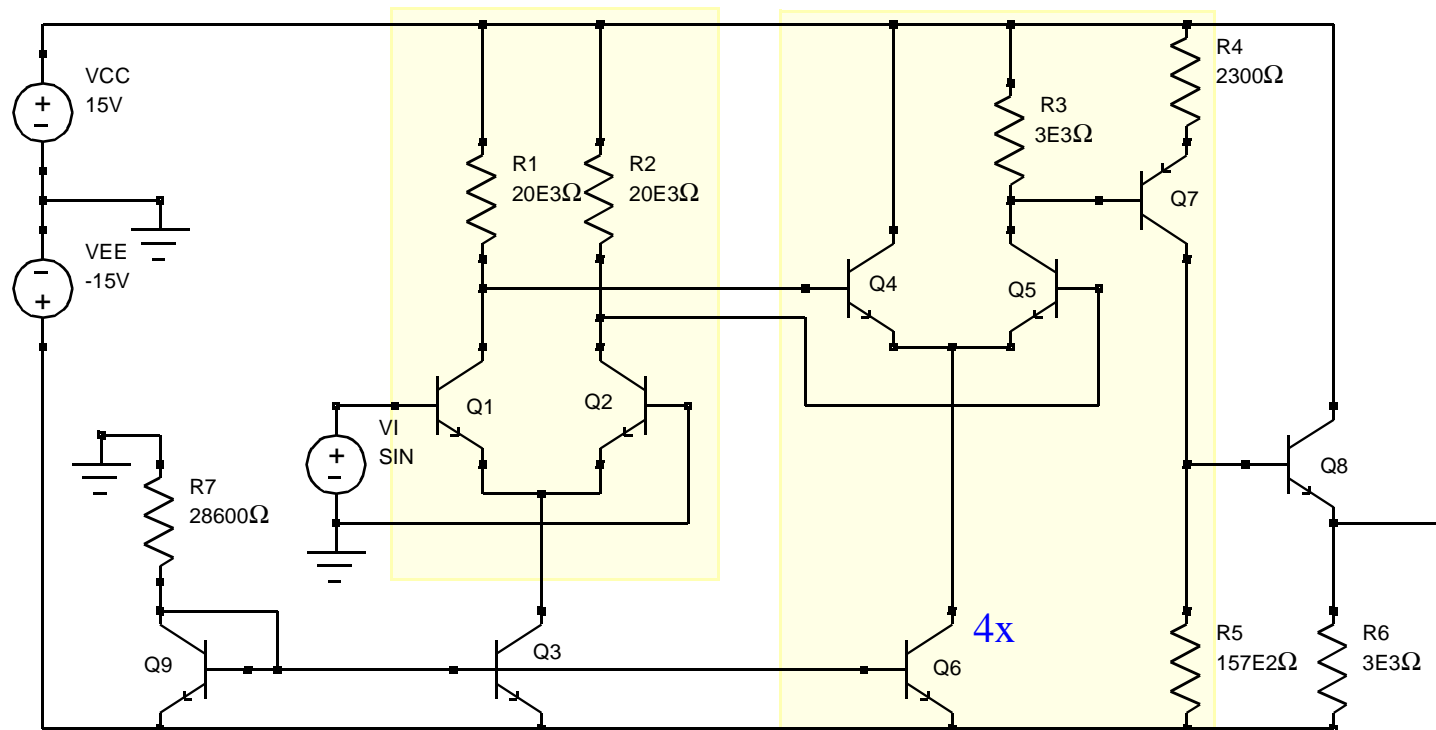
## Beta Dependence

- When “steered” to several points, the  $I_o$  dependence on  $\beta$  can be a problem



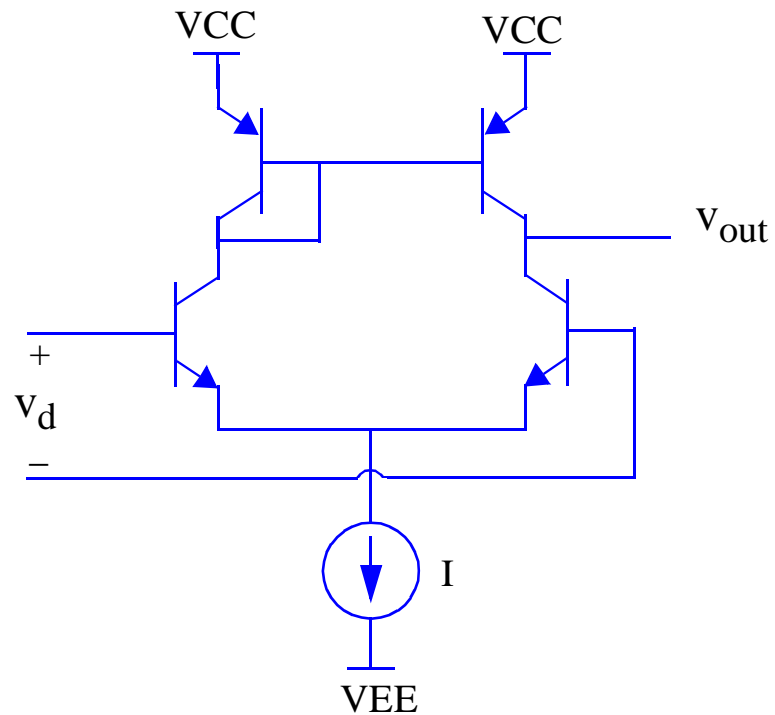
# Simple Opamp Example

- First stage is used to reject common mode voltages
- The 2nd diff amp and level shifting stage provide the gain
- The input diff amp also provides the large input resistance
- Why is Q6 designed to be 4x larger than Q3?



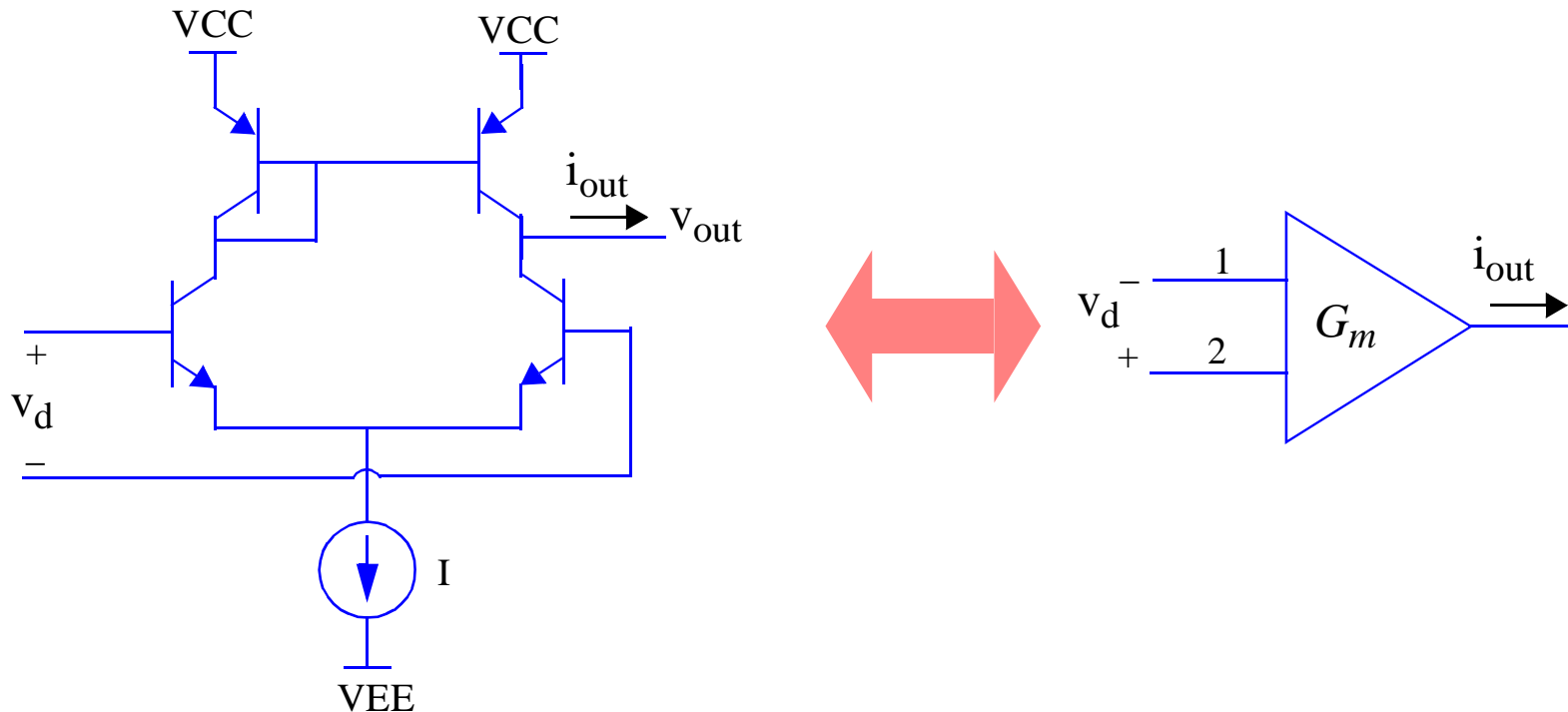
## Differential Amplifiers: Active Loads

- IC resistors are impractical
- Active loads provide current-source-like loads, hence large small signal gains



# Differential Amplifiers: Active Loads

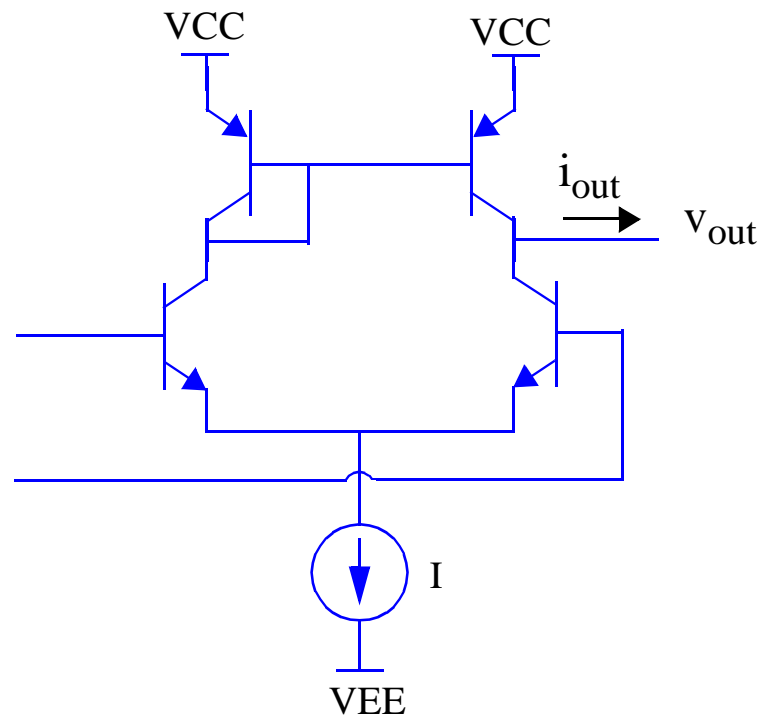
- The output in this example is single-sided, but behaves sort of differentially
- The output is a current, proportional to  $v_d$  --- **transconductance amplifier**



- Assuming infinite  $\beta$ , what is the output current when  $v_d = 0$  ?

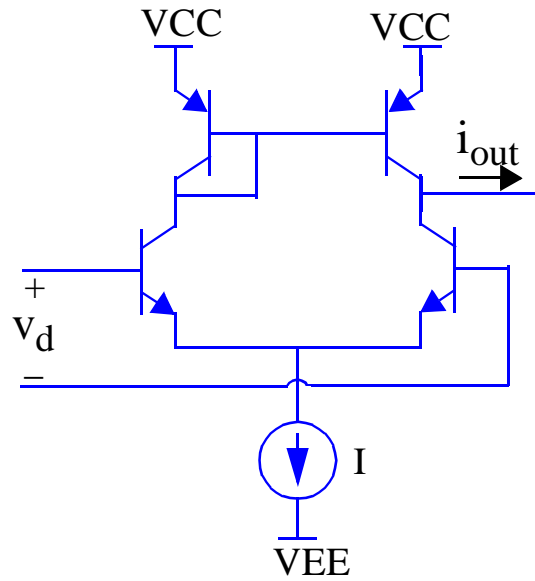
## Common Mode Gain

- If all of the parameter values are exactly matched to one another, and  $\beta=100$ , will there be any common mode gain?



- Will there be any dc offset?

## Small Signal Gain, $G_m$

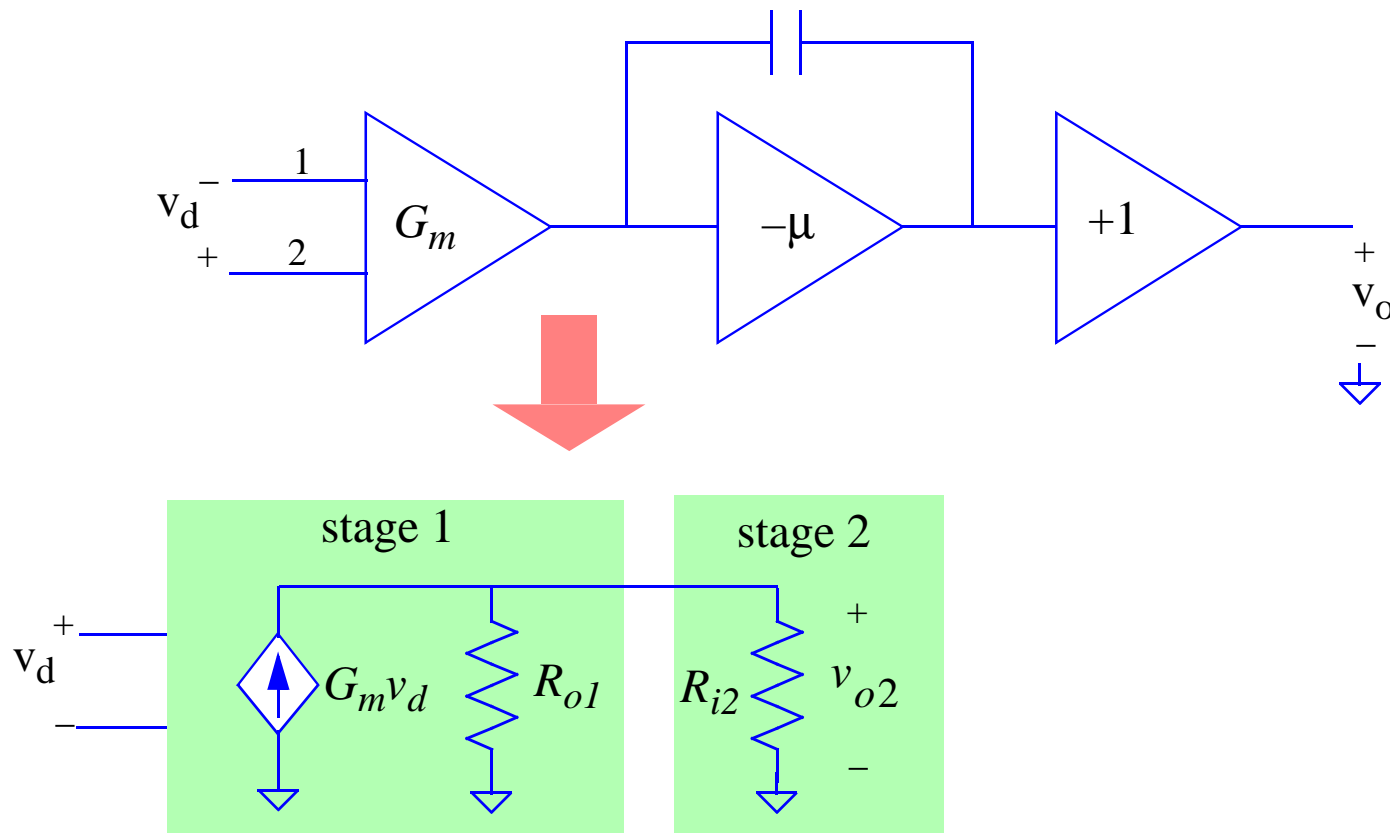




# Small Signal Gain, $G_m$

# Transconductance Stage of Opamp Model

- The voltage gain of stage 1 depends on the output impedance of stage 1 and the input impedance of stage 2



# Transconductance Amplifier Voltage Gain

- Active loads are often designed to maximize  $R_o$

