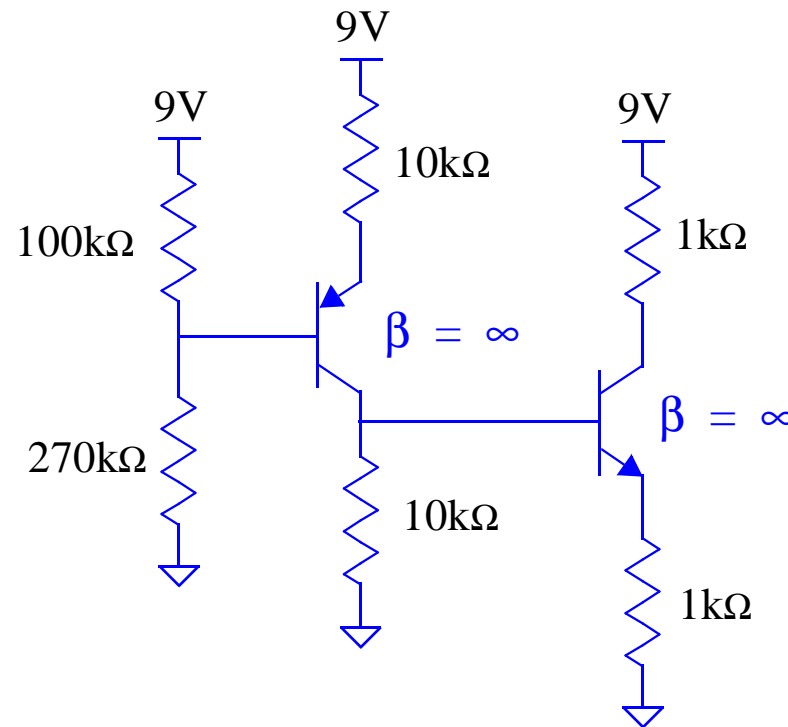


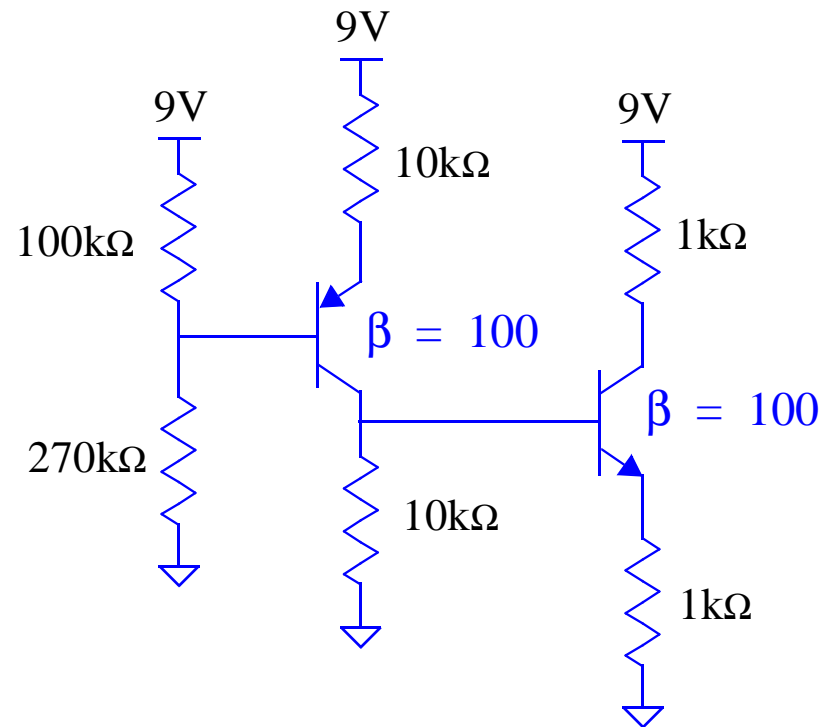
## dc Bias Point Calculations

- Find all of the node voltages assuming infinite current gains



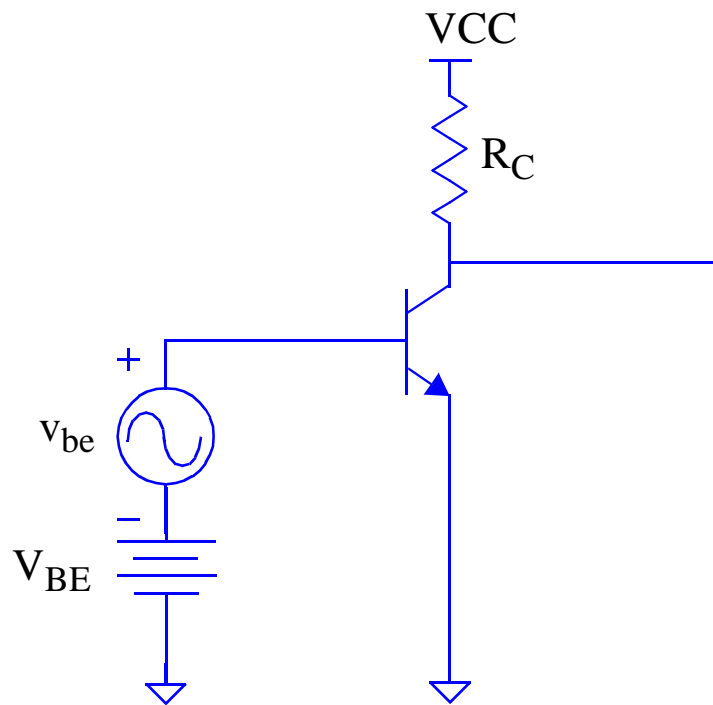
## dc Bias Point Calculations

- Find all of the node voltages assuming *finite* current gains



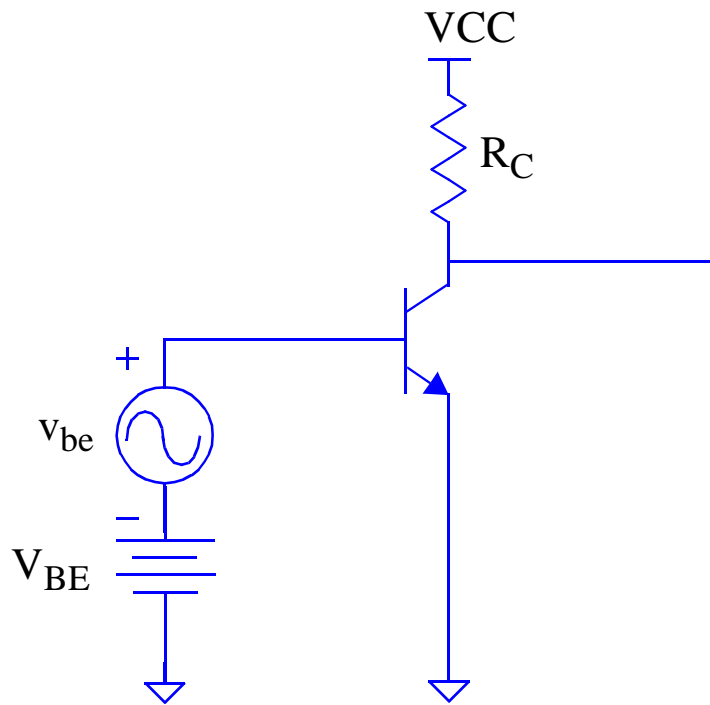
## Biasing and Small Signal Approximations

- Bias the transistor into the linear region, then use it as a linearized amplifier for small ac signals
- Select  $R_C$  so that the transistor will not saturate:



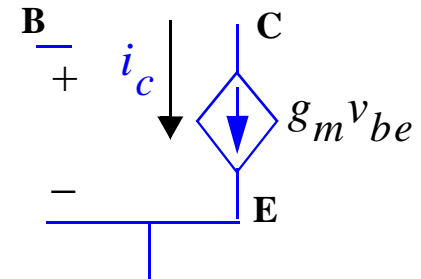
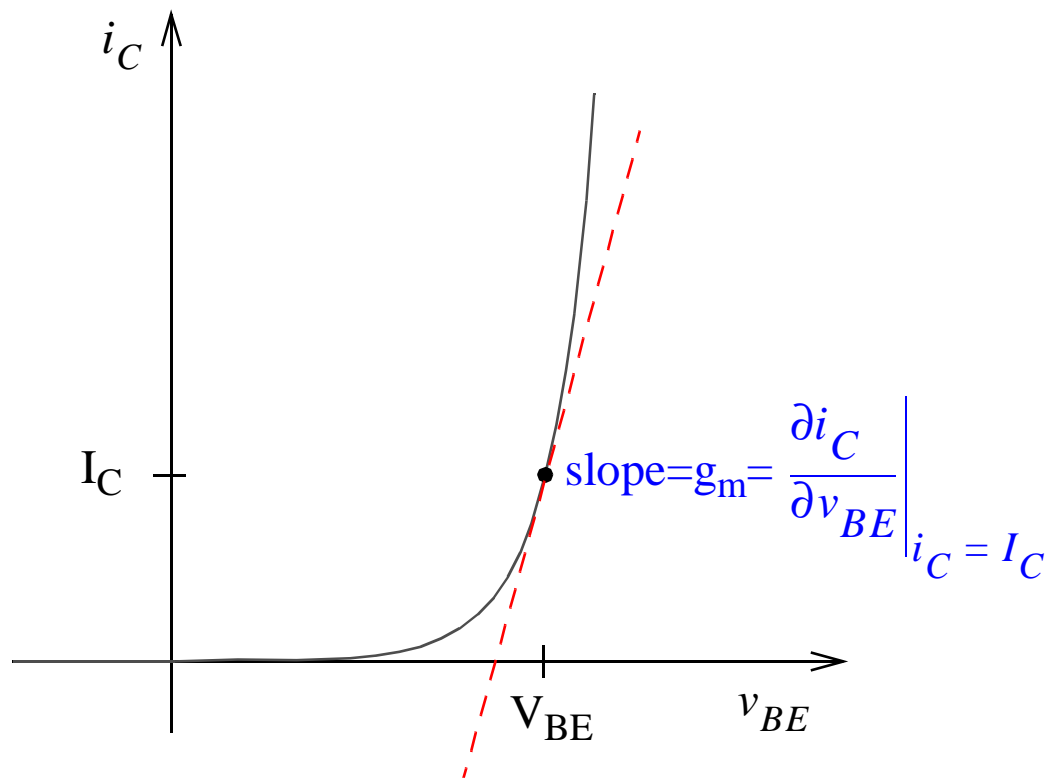
## Small Signal Approximations

- $v_{BE} = V_{BE} + v_{be}$ ;  $i_C = I_C + i_c$  [Note the variable notation]



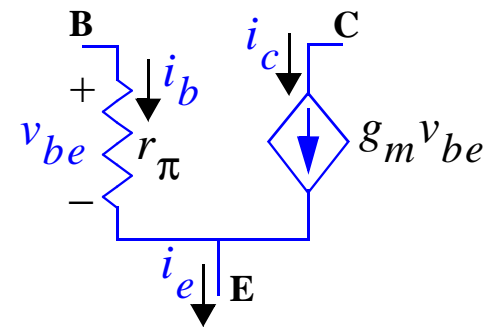
# Transconductance

- Small signal amplifier behaves like a linear voltage controlled current source
- Bias to a value of  $I_C$  to establish the **transconductance**,  $g_m$ , that you want



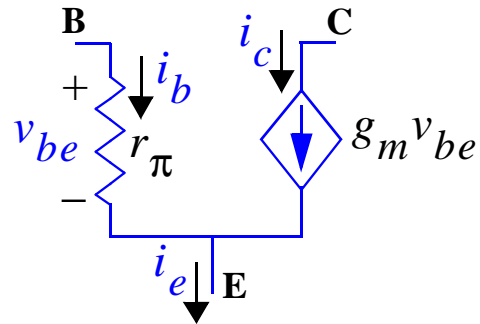
# Input Impedance

- How do we model the small signal behavior as viewed from the input signal?
- What is the small signal change in  $v_{be}$  due to a small signal change in  $i_b$ ?



# Emitter Impedance

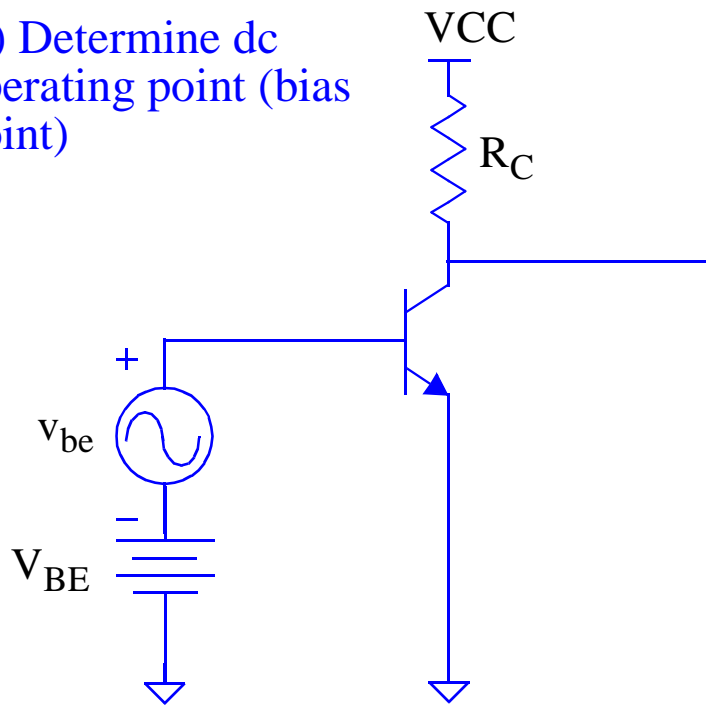
- What is the impedance “seen” by the emitter?



# Small Signal Analysis

- Every response voltage and current has a dc component and a small signal (steady state) component
- dc sources cause the dc portion of the responses
- ac sources cause the ac portion of the responses
- Example:

1.) Determine dc operating point (bias point)

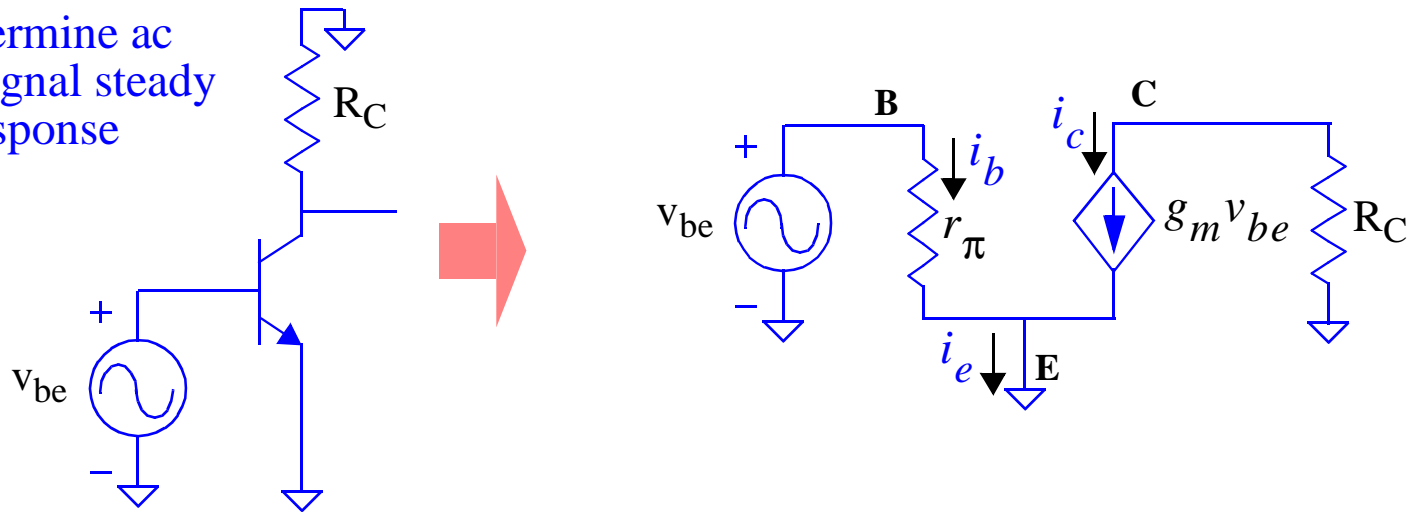




# Small Signal Analysis

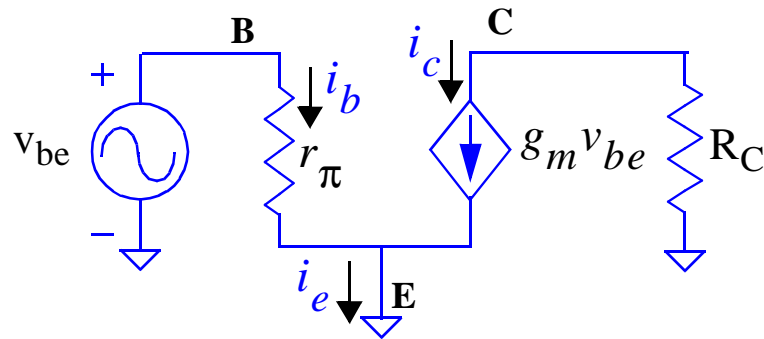
- Then the ac portion of the response can be determined with all of the dc sources removed:

2.) Determine ac small signal steady state response



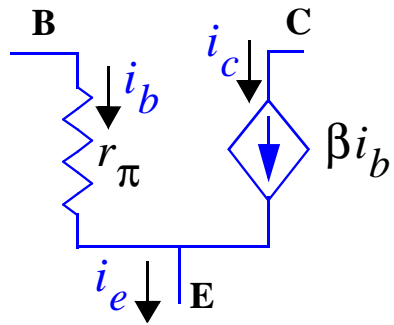
# Small Signal Analysis

- Models **linearized approximation** of ac response about dc operating point
- Calculating  $i_b$  and  $i_c$  is sufficient, but we know that  $i_e = v_{be}/r_e$

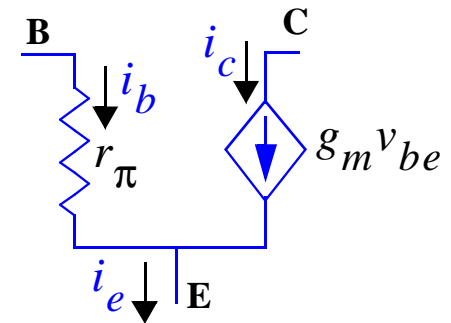


# Hybrid- $\pi$ Small Signal Model

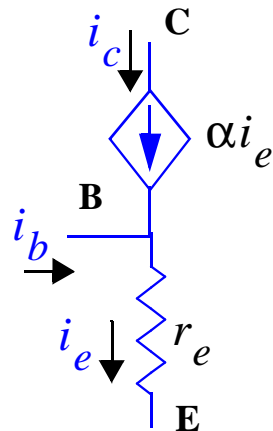
- Another way to represent the amplification of the input signal



Identical in behavior

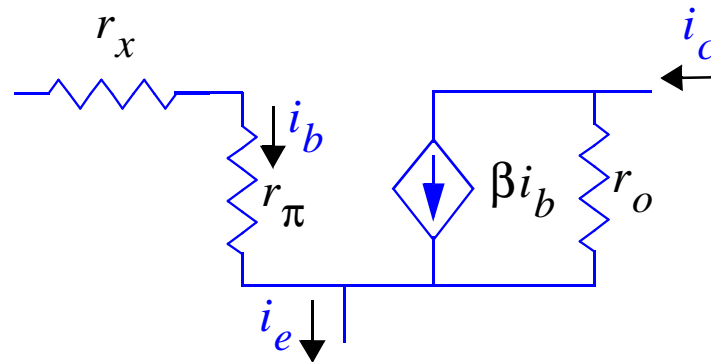


- Or, use  $i_c$  and  $i_e$  to specify  $i_b$



## Small Signal Model

- Some other parameters may be base-resistance and C-E resistance due to Early voltage



- At high frequencies we would have to include the impedances due to the parasitic capacitors

## Small Signal Capacitance Models

- At high frequency we must also model the parasitic capacitances
- The stored based charge is modeled by a diffusion capacitance
- Although it is nonlinear, the small signal diffusion capacitance is linearized about the operating point

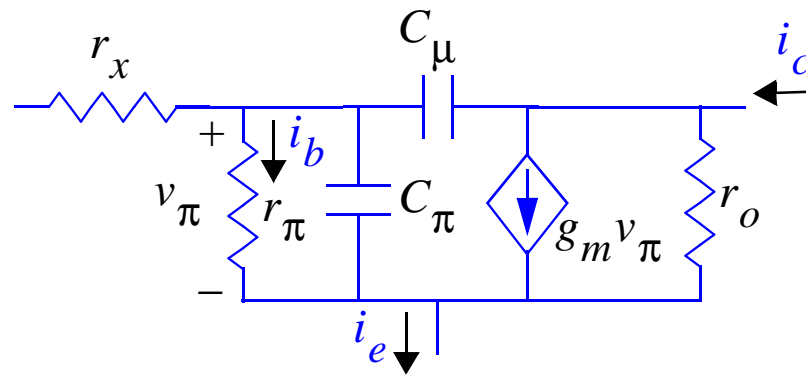
$$Q_n = \tau_F i_C \quad \longrightarrow \quad C_{de} = \tau_F \left. \frac{di_C}{dv_{BE}} \right|_{i_C = I_C}$$

- There are also junction capacitors between emitter-base and base-collector

$$C_{je} = \frac{C_{je0}}{\left(1 - \frac{v_{BE}}{v_{0e}}\right)^m} \quad \longrightarrow \quad C_{je} \cong 2C_{je0}$$

$$C_{jc} = \frac{C_{jc0}}{\left(1 - \frac{v_{BC}}{v_{0c}}\right)^m} \quad \longrightarrow \quad C_{jc} \cong 2C_{jc0}$$

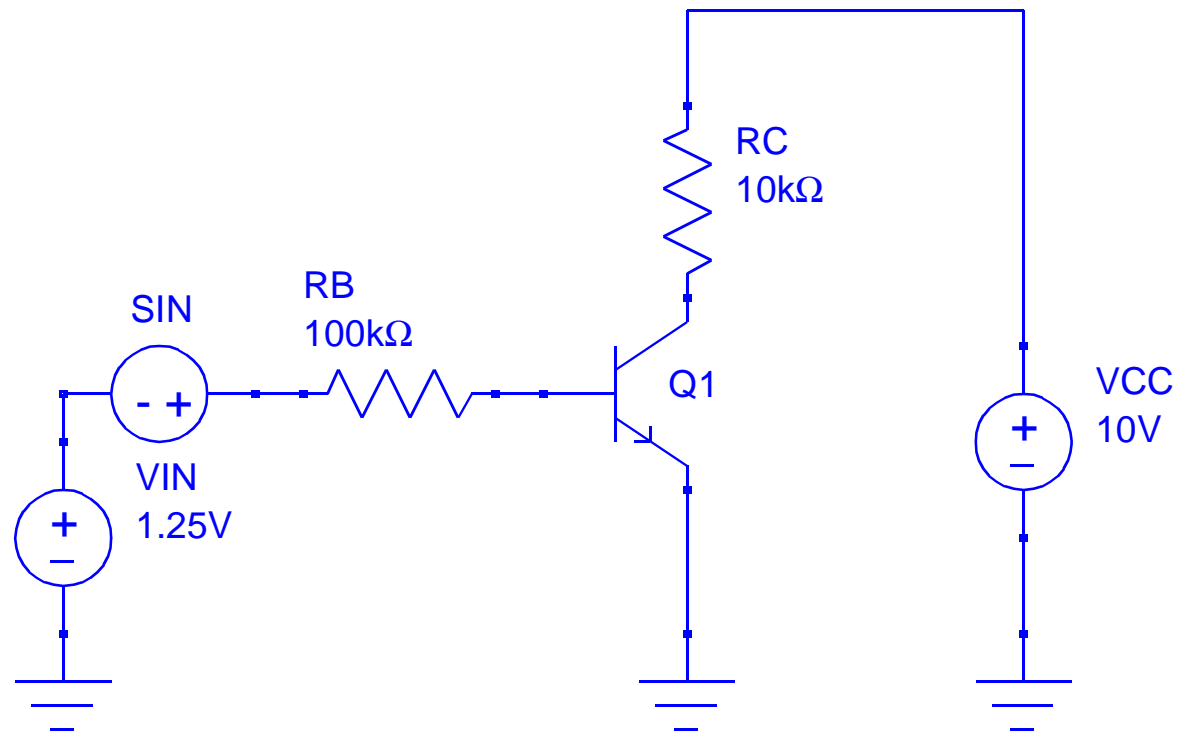
## High Frequency Hybrid- $\pi$ Model



- Ground the emitter, short the collector to the emitter, and drive the base
- Calculate current gain as a function of frequency to define **unity gain bandwidth** of the transistor

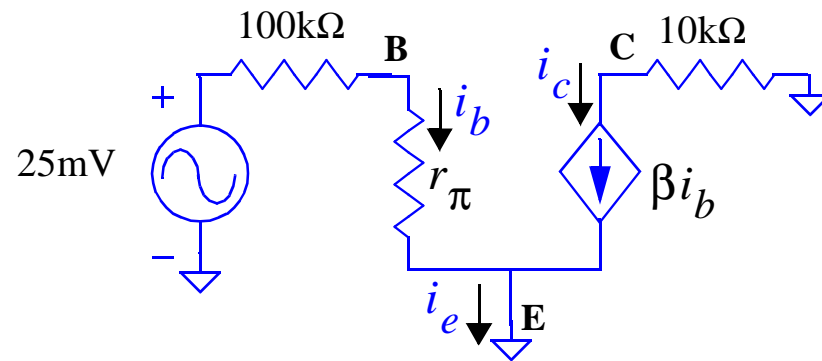
## Example

- Analyze the small signal steady state response



## Example

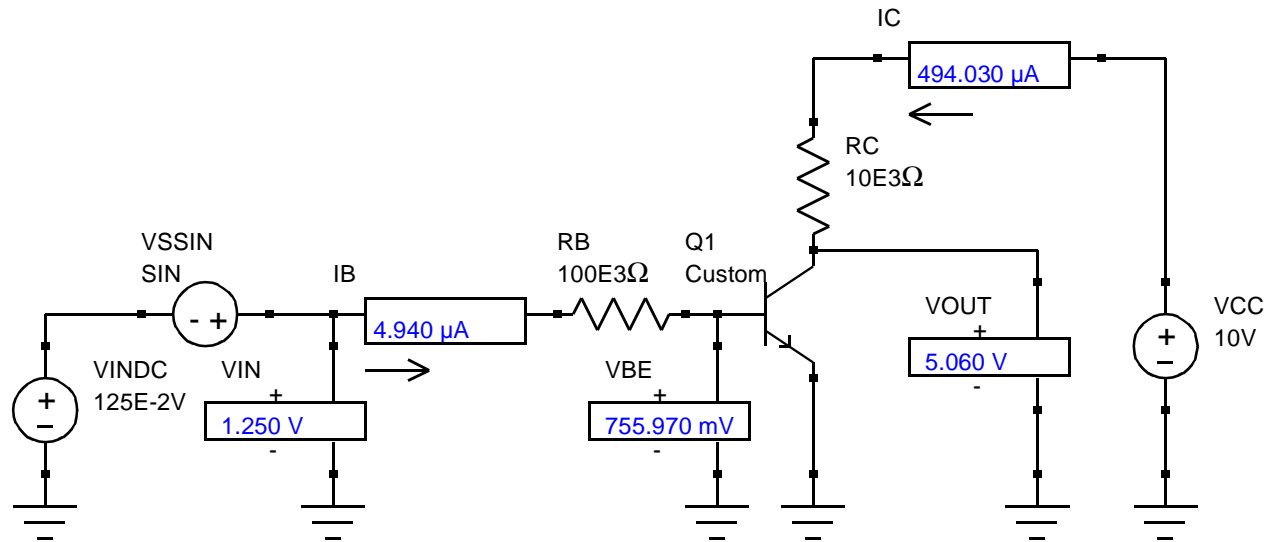
- The gain is easily identified from the small signal model
- For a common emitter configuration, the hybrid- $\pi$  model is the easiest to analyze





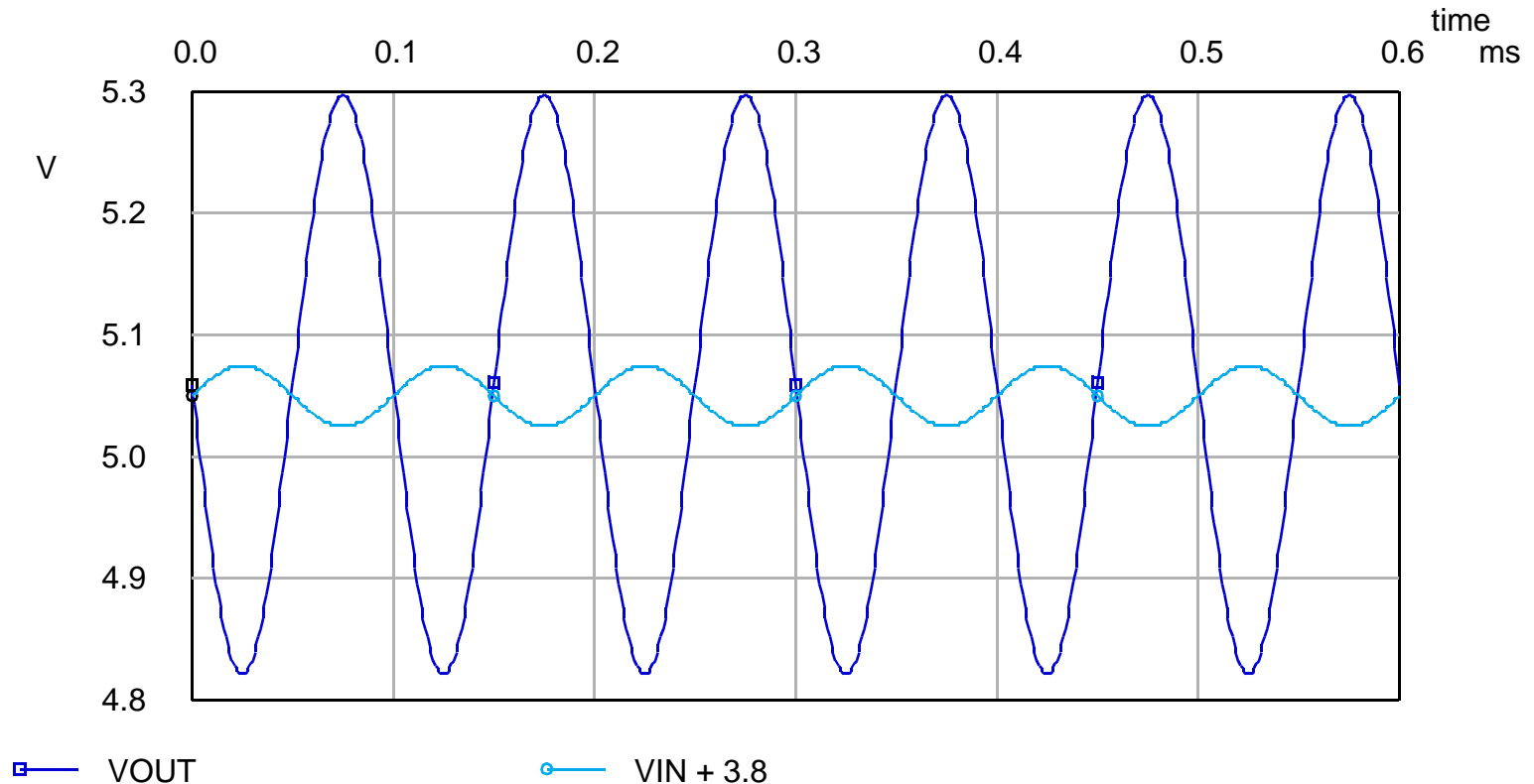
# SPICE Result

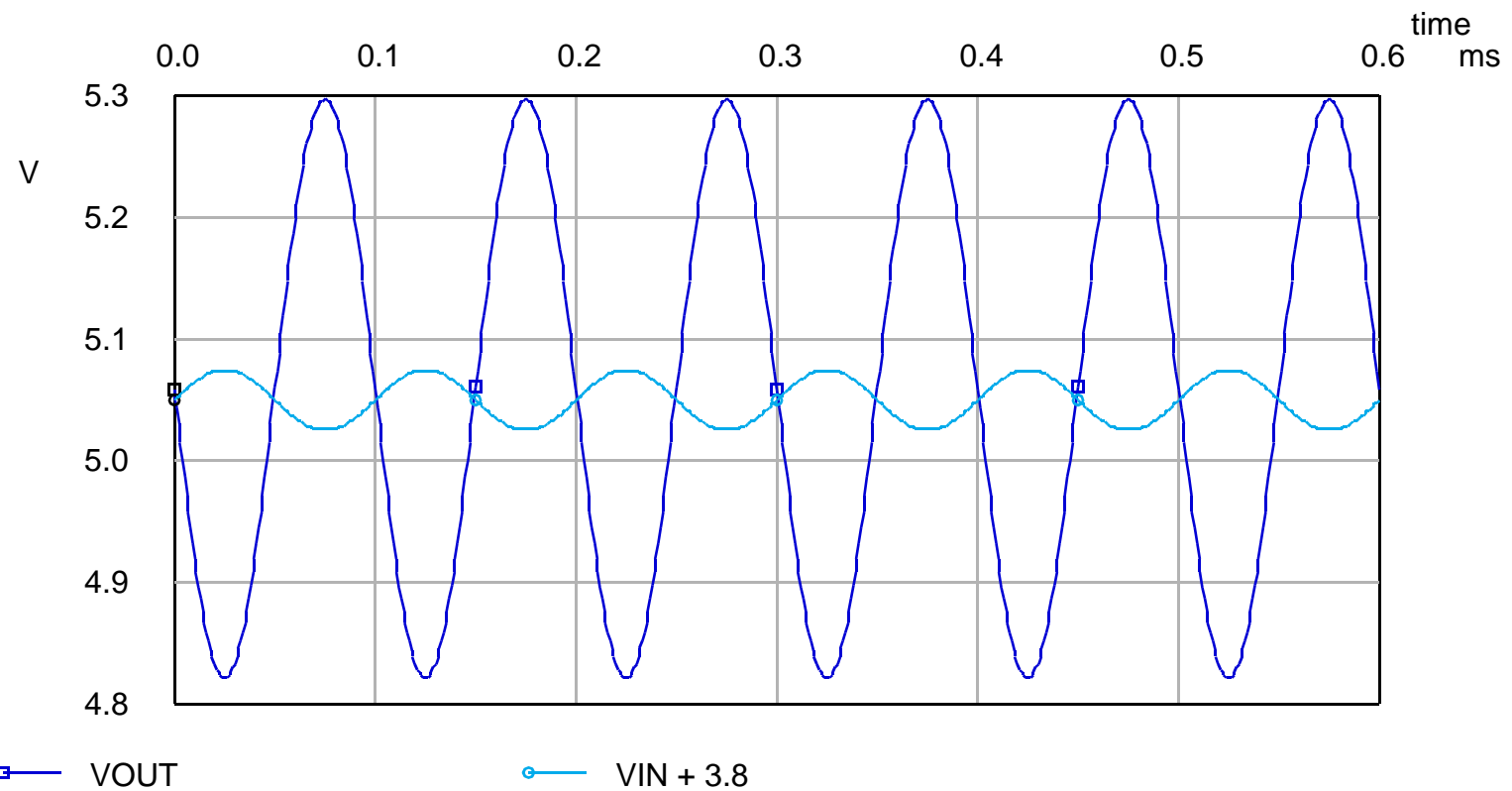
- Bias point solution from SPICE



## SPICE Result Time Domain SPICE Result

- For this example we can perform a transient analysis to get a reasonable approximation of what the steady state sinusoidal response looks like. Why?
- Why is there a phase shift between input and output?

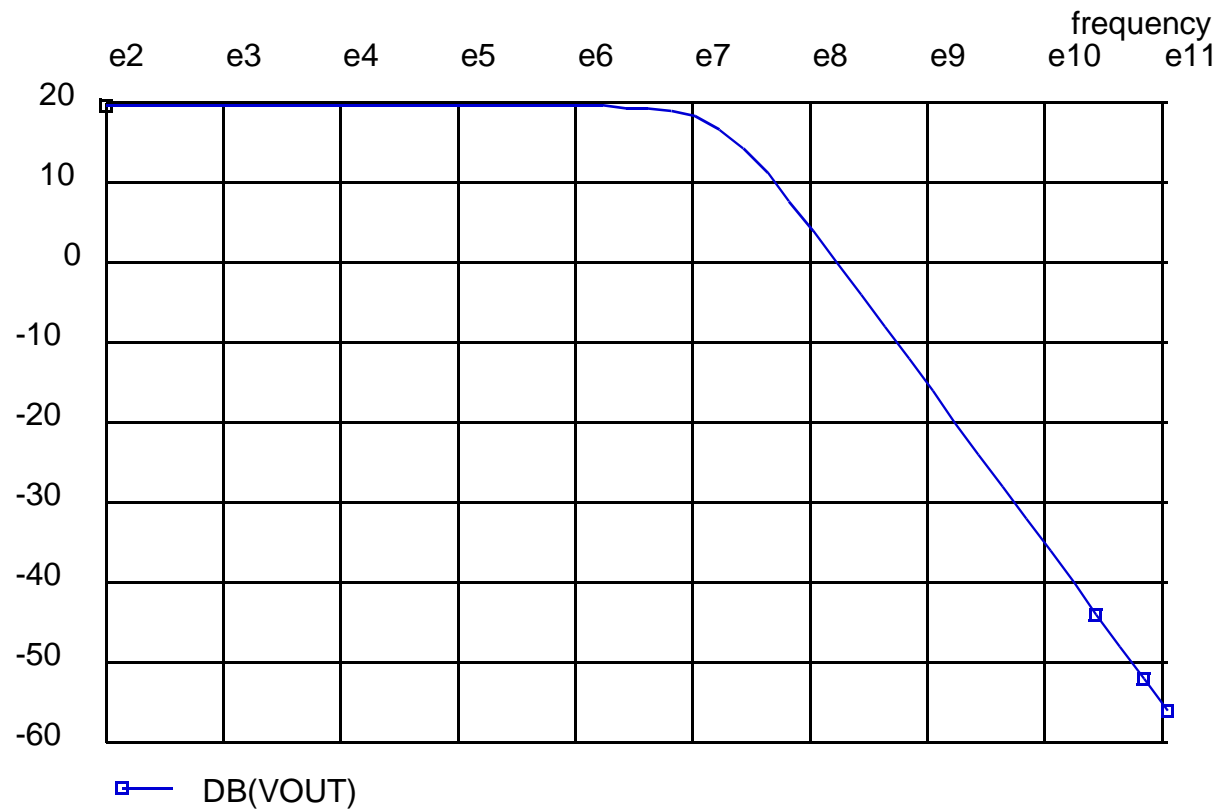




- Is the circuit really behaving like a linear amplifier?
- What does the ac *small signal* frequency response look like?

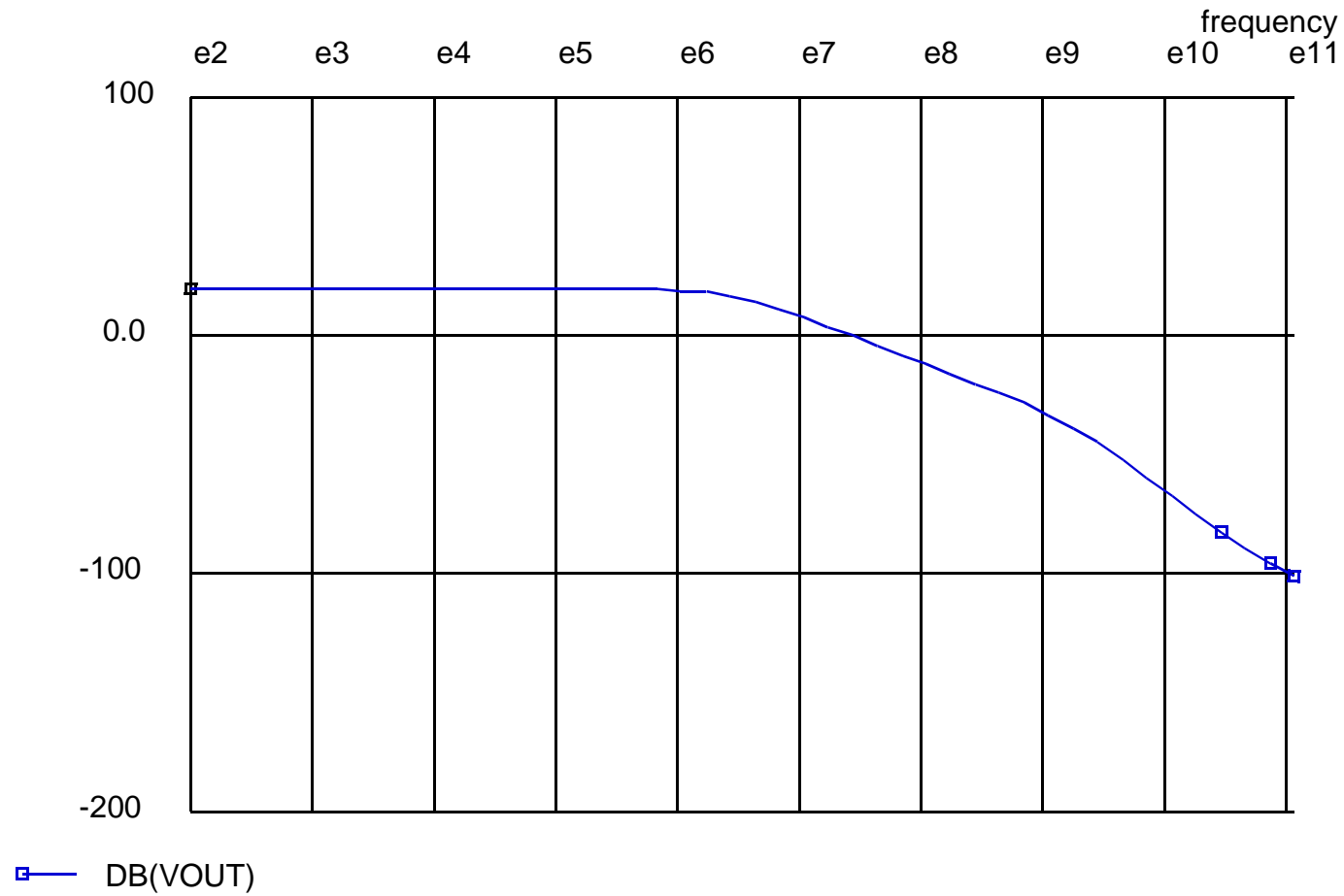
# SPICE Frequency Response

- We have to add the parameters to the SPICE model which represent the capacitance effects before we can observe them in the ac analysis
- e.g.  $TF = 0.1ns$  --- *Diffusion Capacitance*



# SPICE Frequency Response

- Also adding  $CJE = 0.1\text{pF}$



## SPICE Frequency Response

- Small signal models must include capacitance and transit times when we are interested in high frequency responses
- These capacitors are nonlinear, but treated as linearized values about their dc operating point (same as transconductance, etc.)
- The default SPICE model may not even include these parameters since it unnecessarily complicates the model for a simulation of the mid-band frequencies
- For the mid-band frequency range of interest we can view these capacitors as open